

An Optimization Method For Planar Transformer Winding Losses In GaN Based Multi-output Flyback Converter

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Outlines

- Background
- The Analysis Method of Winding Losses for Multi-Output Flyback Converter (MOFC) Planar Transformers
 - The analysis method for MOFC Planar Transformer's winding loss
- Winding Design and Optimization of MOFC Planar Transformers
 - Winding design of dual-output Flyback planar transformers
 - A novel design of winding structure for MOFC planar transformers
- Experimental Results
- Summary

Benefit of Multi-Output Flyback



Requirements:

- Multi-Outputs with Different Voltage Levels
- □ Smaller Size and Weight
- Higher Efficiency





- J Low Cost, Simple Structure
 - Few Components Count

Benefit of Planar Transformers



The Analysis Method of FB Planar Transformer`s Winding Loss



The Analysis Method of FB Planar Transformer's Winding Loss





The total winding loss is the sum of the transformer part and the inductance part.

 $i_{\rm p}(t)$ $i_{\rm s}(t)$ $P_{\text{windingLoss}}$ **Opposite-Phase** $i_{p_Tx}(t)$ $i_{\rm s Tx}(t)$ windingLoss Tx Transformer Component Same-Phase $i_{\rm s \ L}(t)$ $i_{p_L}(t)$ $P_{\text{windingLoss}_L}$ Inductor Component

The Primary and the Secondary Current in DCM

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The Analysis Method of MOFB Planar Transformer's Winding Loss



Winding Design of A Dual-Output FB Planar Transformers

78W Dual-output FB



Cross-Section of the Planar Transformer



■ Main circuit: Dual-output QR Flyback ■ Input voltage: 90-264Vac ■ V_{o1} =12V, I_{o1} =2.4A, V_{o2} =120V, I_{o2} =0.4A ■ N_p : N_{s1} : N_{s2} =14:1:9 **Based on minimizes DC winding loss :**

$$\frac{I_{o1} + I_{o2}}{S_{ws1}} = \frac{I_{o2}}{S_{ws2}} = \dots = \frac{I_{o2}}{S_{ws10}}$$

Winding Design of A Dual-Output FB Planar Transformers

Magnetic Field Distribution of the Winding Structure



Time-Domain Graph of Winding Loss





□ The total winding loss is high.

The Equivalent Magnetic Circuit of Transformer Core

MMF Core Magnetic Potential Difference F $\Phi_{a|2}$ Φ_{a_n} 2 ••••• Height F/2Length A2 Length \square $R_{a 2} \sim R_{a n}$: Reluctances between the $R_{a_2} \sim R_{a_n} \downarrow \Box \qquad \phi_{a_2} \sim \phi_{a_n} \uparrow$ Eddy Current \Box Magnetic Core Window Height $\square \phi_{a_2} \sim \phi_{a_n}$: Stray Flux OSS

Variation of MMF along the Core Structure



Conductors can impede alternating magnetic fields.

Cross-Section of the Improved Winding Structure



Magnetic Field Distribution of the Improved Winding Structure





Time-Domain Graph of Winding Loss



Winding Structure	Unimproved	Improved
Average	2.415W	1.588W



Unimproved Winding Structure



Improved Winding Structure





Winding Structure	Core Structure	
	Traditional	Distributed Air- gap
Unimproved	2.415W	1.25W
Improved	1.588W	1.07W

78W Dual-Output TV Power Supply



Size: $60.5 \times 93.6 \times 14.5$ mm³ High Stability and Low Cost



Benefit of GaNSense Control: NV958X



The Efficiency of Different Transformers

Traditional Core Structure:

- Unimproved Winding Structure
- Improved Winding Structure

Distributed Air Gap:

- --- Unimproved Winding Structure
- --- Improved Winding Structure
- In traditional Core, the improved winding structure get a 1.2% increase.
- In distributed air gap, the improved winding structure get a 0.3% increase.



Temperature of Different Planar Transformers

Traditional Core + Unimproved Winding

Max Temp 130.5



Traditional Core ♣ Improved Winding

Max Temp 118.5



Distributed Air Gap ♣ Unimproved Winding

Max Temp 104.8



Distributed Air Gap ♣ Improved Winding

Max Temp 103.7



Summary

- In the MOFC, the proposed winding optimization method significantly reduces winding losses in planar transformers without increasing additional costs.
- Utilizing the flat magnetic core structure with distributed air gaps not only reduces air gap leakage flux, but also significantly decreases stray flux, resulting in a substantial reduction in winding losses.